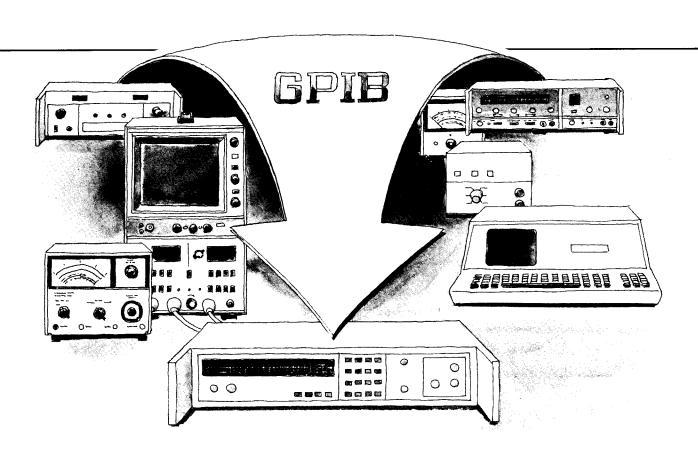


APPLICATION NOTE #203

GPIB CONTROL OF NON-GPIB SIGNAL SOURCES

Fully automatic test and measurement systems, usually called Automatic Test Equipment (ATE), are becoming increasingly important in improving efficiency. A single controller can supervise the operation of a full complement of instruments which are all connected to a General-Purpose Interface Bus (GPIB). Such a system can make a great many measurements quickly and accurately—without the constant attention of highly skilled and highly paid technical personnel.



The ATE Designer's Problem

The IEEE standard covering the GPIB was introduced in 1975. Although its value was quickly apparent, it took time for manufacturers to design and build equipment to accommodate GPIB control. The first available equipment, of course, was the simplest to adapt to digital control—such instruments as digital voltmeters and frequency counters. Complex analog devices, such as microwave sweep generators, were among the last to be offered with GPIB control capability.

Such signal sources have always been expensive, and the new GPIB-controlled versions cost even more. Since many companies have large investments in sweepers which cannot be retrofitted for GPIB control, some ATE designers have resorted to "stopgap" measures to make use of existing equipment.

For example, Figure 1 shows a GPIB-controlled frequency counter combined with a D/A converter to form a frequency-control loop. The software must be set up so the controller can issue instructions, read the result, then repeat the process until the desired frequency is achieved. The arrangement works, but it is quite slow, and it provides limited frequency accuracy. It is used simply because the cost of available alternatives is too high.

Another problem facing the ATE designer who is involved with microwave frequencies is the rapid move to higher frequencies. While 18 GHz was recently considered a high frequency, signals of 100 GHz and above are not uncommon now. Sources operating at these frequencies seldom include GPIB control. Moreover, the solid-state sources that operate in the millimeter-wave region are typically quite unstable. They can vary by tens of megahertz in a few seconds. As a result, this new frequency area, with the limited availability of signal sources, presents a special challenge to the ATE designer.

Cost-Effective Solution

EIP Microwave has developed a simple, easily implemented way to

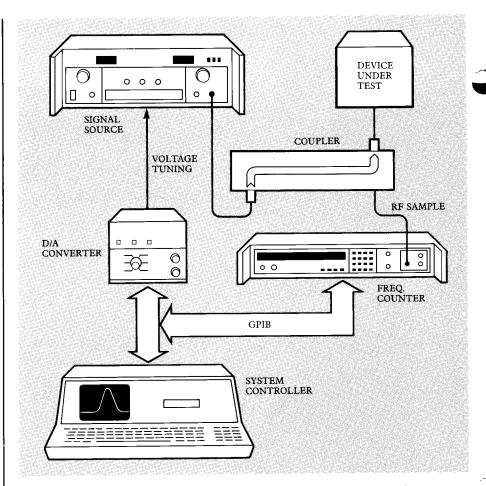


Figure 1. Software frequency-lock loop suffers from slow operation and limited frequency accuracy.

put the frequency of virtually any electrically controllable microwave source under GPIB control. The only additional equipment required is an EIP Model 575 or 578 source-locking frequency counter. (The primary difference between the two models is the frequency range: 10 Hz to 18 GHz for the 575, and 10 Hz to 110 GHz for the 578.) Since the cost of one of these counters is a fraction of what a new sweeper would cost, the savings can be substantial.

As Figure 2 indicates, only three cables between the counter and the signal source are required to permit the counter to exercise full frequency control over the source. One cable provides a sample of the RF output to the counter, while the other two carry the coarse-tune and phase-lock commands to the sweeper. The system controller supervises the counter through its built-in interface.

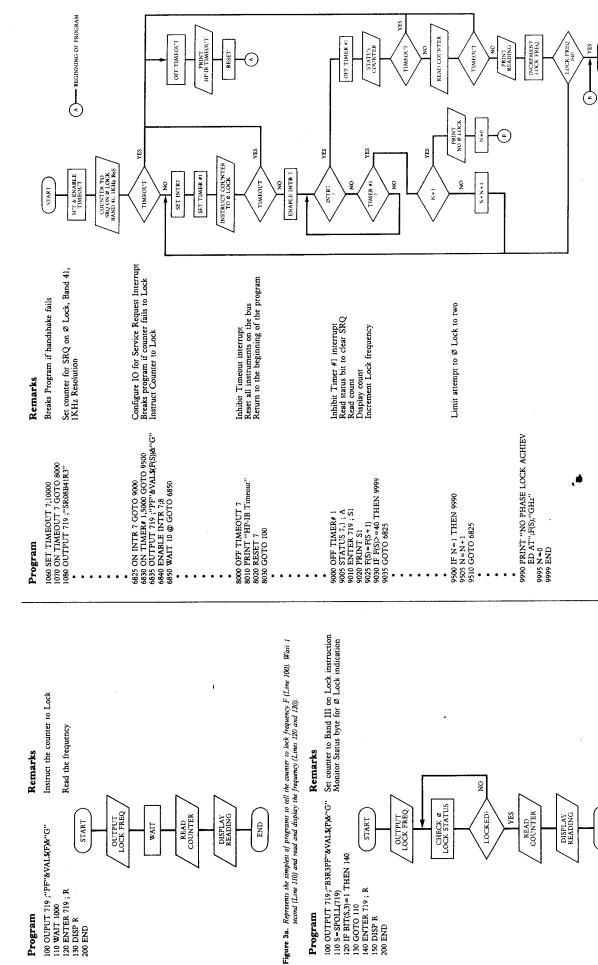
The only necessary GPIB commands are instructions to the counter. And the only monitoring required of the con-

troller is to check the lock status bit from the counter. The results that can be obtained with existing signal sources are dramatic, in terms of both speed and accuracy.

In contrast, the frequency-loop arrangement of Figure 1 requires the controller to communicate directly with the signal source and the counter.

Flexibility in equipment arrangements is another advantage of using the source-locking counter. Since the only software instructions issued by the controller are those to the counter, signal sources can be easily changed to meet new requirements. A new source can be put into the ATE system simply by connecting the three cables to the counter.

Of course, this interchangeability also offers software standardization among all ATE systems that use source-locking counters. The HP-85 subroutines shown in Figure 3 apply, regardless of the signal source used in a particular system.



Remarks

100 OUTPUT 719;"B3R3PF"&VAL\$(P)&"G"

0

Program

Read the frequency

100 OUPUT 719 ,*PF*&VAL&F)&*G**
110 WAIT 1000
120 ENTER 719 ; R
130 DISP R
200 END

į...

OUTPUT LOCK FREQ.

READ COUNTER

WAIT

DISPLAY

END

Remarks

Program

Figure 3b. Represents a program with minimum time of execution for a lock at a specific frequency. F thru the use of serial Poll to cheek for Ø Lock (Line 110 and 120).

S Z

LOCKED?

READ COUNTER

DISPLAY READING

END

YES

CHECK Ø LOCK STATUS

OUTPUT LOCK FREQ.

START

110 S=SPOLL(719)
120 IF BIT(S,3)=1 THEN 140
130 GOTO 110
140 ENTER 719; R
200 END

Figure 3c. Represents a portion of a complex system program with precautions taken to deal with problems in the handshake routine and failure to achieve a Phase Lock. This program also implements the Service Request function to indicate when Phase Lock has been achieved.

END

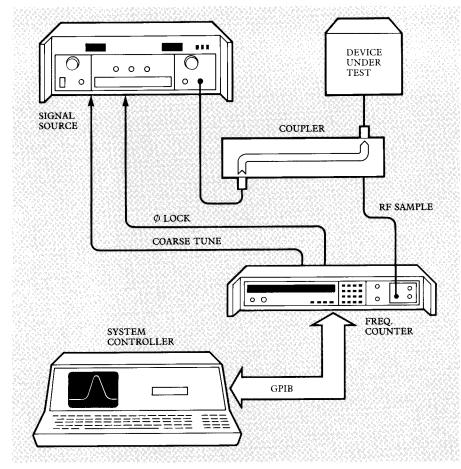


Figure 2. Source-locking loop uses EIP 575 or 578 counter to provide rapid response and frequency accuracy equivalent to counter's time base.

Added Value

Source locking is only one function of the 575/578 counters. They not only offer the flexibility of general-purpose counters, but they include other capability (also under GPIB control) that might otherwise require additional instruments:

- Optional power measurement provides the simultaneous measurement of signal frequency and power.
- 2. A frequency-limiting feature permits spectral analysis. Both the frequency and power of individual signals can be measured in a multi-signal environment—even when unwanted signals are stronger.

Such capability, combined with a frequency range of up to 110 GHz, offers the ATE designer almost unlimited possibilities.

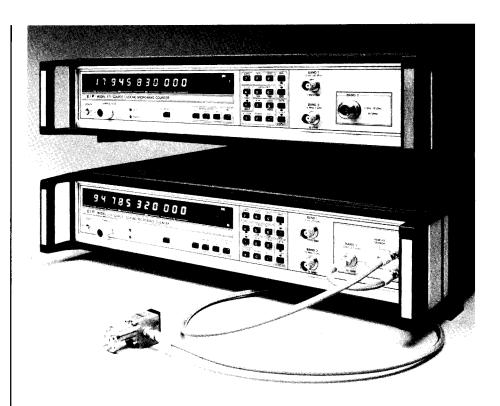
More Information

EIP Microwave publishes application notes on a variety of subjects involving high-performance counters. And an applications-engineering staff is available to provide advice and answer specific questions. For more information, contact EIP or any EIP representative.

Performance

The accompanying specifications show the basic source-locking performance of the 575 and 578 counters. Most microwave sources (even the older ones) meet the counter's requirements. This provides an opportunity to extend the useful life of equipment that might otherwise be considered obsolete.

Since most microwave sweepers provide poor frequency accuracy, some applications require a very expensive synthesizer. Now the same accuracy can be achieved by putting an ordinary sweeper under the control of a source-locking counter. Then the frequency accuracy becomes as good as the counter's time base. With the standard 575/578 time base, this means short-term accuracy of one part in 109. The optional oven-controlled time base offers accuracies of up to one part in 1011. While the source-locking arrangement does not transform an ordinary sweeper into a synthesizer, it approximates much of the synthesizer's costly performance.



EIP's 575/578 series counters combine frequency measurement and source locking capability to 110 GHz.

SOURCE LOCKING SPECIFICATIONS

Frequency Range 10 MHz-Max. capability of counter.

Resolution 10 kHz for phase lock freq.

≥ 50 MHz

2.5 kHz for < 50 MHz

Accuracy Equal to counter's Time Base
Long Term Stability Equal to counter's Time Base

Minimum Phase Lock

, Signal Level Equal to counter sensitivity
Polarity Automatically selected

Bandwidth User select, 10 kHz, 2 kHz or 500 Hz, or automatically selects widest

bandwidth capable of locking.

LOCK TIME (Typical)

Coarse Tune 50 m sec + 1 counter aquisition

time for source bandwidth greater than 100 Hz; limited by source tuning speed below 100 Hz.

Phase Lock 200 m sec

Recall Stored Data 1 counter aquisition + 100 m sec limited by source tuning speed.

OUTPUT DRIVE

(Maximum)

Coarse Tune Output + 10 V into 5 K ohm min.

Phase Lock Output ±10 V into 5 K ohm min for source

gain constant <64 MHz/V. ±75 MA into 10 ohm max for source gain constant <3.2 MHz/MA.

±.6 V into 5 K ohm min for source gain constant ≥64 MHz/V.

 ± 4.5 MA into 10 ohm max for source gain constant ≥ 3.2

MHz/MA.

CAPTURE RANGE

Coarse Tune Entire range of selected counter

band limited by maximum output

drive.

Phase Lock Source gain constant X maximum

output drive.

OUTPUT CONNECTOR

Coarse Tune Rear panel BNC, female Phase Lock Rear Panel BNC, female

PHASE LOCKED

SPECTRUM (See figure below) -

Noise Floor vs Input Frequency:

The noise floor extends from the carrier to approximately the loop bandwidth. Beyond this the noise floor decreases 12 dB/bandwidth octave. The noise floor is the greater of:

1. NOISE FLOOR = .70 dBC/Hz

2. NOISE FLOOR = (20 log F -65) dBC/Hz where F = Input frequency in GHz

REQUIRED SOURCE CHARACTERISTICS

External Sweep (Coarse Tune) Input:

Bandwidth 5 Hz minimum

Tuning Sensitivity 10 MHz/V minimum; 10 GHz/V maximum

FM (Phase Lock) Input:

Bandwidth

2 kHz minimum

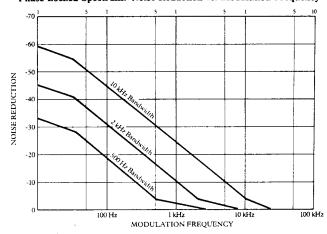
Tuning Sensitivity
Voltage Driven Input

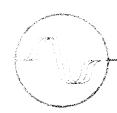
±2 MHz/V minimum ±1000 MHz/V maximum

Current Driven Input ±0.1 MHz/mA minimum

±50 MHz/mA maximum

Phase Locked Spectrum: Noise Reduction vs. Modulation Frequency





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